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# Chemical identification and determination of sulfonamides in *n*-component solid mixtures within THz-region—Solid-state Raman spectroscopic and mass spectrometric study

M. Lamshöft, B.B. Ivanova\*, M. Spiteller\*

Institute of Environmental Research, University of Dortmund, Otto-Hahn-Strasse 6, 44221 Dortmund, Germany

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#### ABSTRACT

The identification and quantitative determination of sulfonamidesin solid-state as n-component mixtures is performed. The limits of detection (LODs), accuracy, precision and repeatability are obtained and discussed, using the Raman spectra within  $200-30\,\mathrm{cm}^{-1}$  region ( $6.00-0.9\,\mathrm{THz}$ ). The excitations, corresponding to H-bonding deformations, lattice vibrations, as well as coupling modes are used for determination. The validation of the statistical and mathematical tools for procedure of the spectroscopic patterns is performed. The possibilities of baseline correction methods, smoothing procedures, and non-linear curve fitting method for quantitative analysis within THz-region for complex spectroscopic patterns of n-component mixtures (n = 1–5) are discussed. The hybrid HPLC tandem mass spectrometry (MS/MS) and powder XRD are applied as independent physical methods for analysis of the studied systems.

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# 1. Introduction

The advantages of the THz-spectroscopy consist of the possibility for nondestructive materials identification and characterization. Thus, allowing application in interdisciplinary areas of the human, health and social science as security, environmental inspection, detection, protection, spectroscopic imaging, biomedical analysis, space communications, tomography imaging, label-free genetic analysis, and chemical/biological sensing and more. The large potential of the method for sensing and identification of chemicals is based on the fact that almost all molecules show spectral characteristics in the THz-region, related to H-bond deformations, skeletal modes, and/or lattice vibrations. Recent study drugs analysis by THz-spectroscopy has been defined the further systematic studies, relating especially the qualitative aspect of the quality control purposes. The THz-region of the electromagnetic spectrum is of great scientific fundamental interest, related the observed linear optical and nonlinear optical phenomena as well [1-22].

Therefore, the presented study aims discussion into two-fold. Firstly, to make parallel between the THz-spectroscopy and solidstate Raman method, for chemical identification. Secondly, to explore the possibility of Raman spectroscopy in a combination with mathematical methods for spectroscopic curve procedure for analysis. Especially, for the quantitative analysis, the solidstate Raman spectroscopy show remarkable for the vibrational spectroscopy LODs of 1.45% using the mid-IR region of the electromagnetic spectrum [23–31]. The application of the method within 6.0–0.9 THz need special attention, because of the lattice vibrations often are characterized with the strong intensity and well define sharp peaks, thus resulting to a possibility for quantitative application and achievement of the better LODs. The object of study is five sulfonamide drugs, characterizing with different level of the overlapping effects of the spectra within THz-region. The advantages of the applied mathematical methods are shown discussing the factors as overlapping effect, intensity, and sharp/broad character of the frequencies. The obtained results illustrate the great capability of baseline correction methods, smoothing procedures and nonlinear curve-fitting methods for study the spectroscopic patterns within THz-region. The obtained data from the non-linear methods are comparing with the classical multiple linear regression method as well as the analysis of variance for multiple linear regressions. The hybrid HPLC/mass spectrometry is used as parallel

<sup>\*</sup> Corresponding authors. Tel.: +49 231 755 4080; fax: +49 231 755 40 85. E-mail addresses: B.Ivanova@infu.tu-dortmund.de, B.Ivanova@web.de (B.B. Ivanova), Spiteller@infu.tu-dortmund.de (M. Spiteller).

independent physical method for separation and characterization of the studied solfonamides.

#### 2. Experimental

#### 2.1. Materials

4-Amino-N-pyridin-2-yl-benzenesulfonamide (1), 4-Amino-N-pyrimidin-2-yl-benzenesulfonamide (2), 4-Amino-N-thiazol-2-yl-benzenesulfonamide (3), 4-Amino-N-(5-methyl-isoxazol-3-yl)-benzenesulfonamide (4) and 4-Amino-N-(3,4-dimethyl-isoxazol-5-yl)-benzenesulfonamide (5) were Sigma-Aldrich products.

#### 2.2. Physical methods

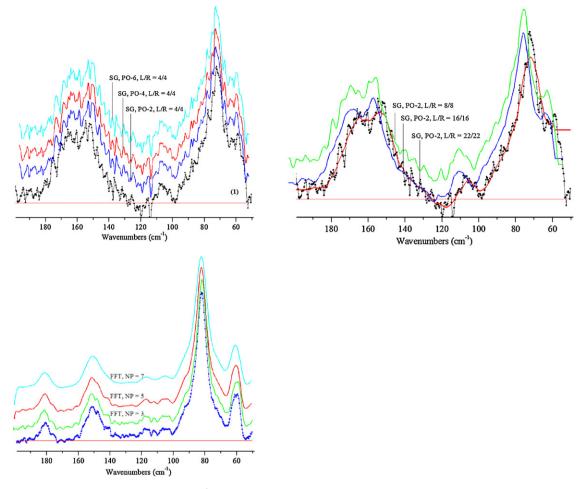
Solid-state Raman spectra were recorded on Nicolet NXR 9610 FT-Raman spectrometer at ambient conditions ( $T = 298 \,\mathrm{K}$ , P = 1 atm). HPLC-MS/MS measurements were performed, using TSQ 7000 instrument (Thermo Electron Corporation). Two mobile phase compositions were used: (A) 0.1% (v/v) aqueous HCOOH and (B) 0.1% (v/v) HCOOH in CH<sub>3</sub>CN. Electrospray ionization (ESI) mass spectrometry. A triple quadrupole mass spectrometer (TSQ 7000 Thermo Electron, Dreieich, Germany) equipped with an ESI 2 source was used and operated at the following conditions: capillary temperature 180 °C; sheath gas 60 psi, corona 4.5 µA and spray voltage  $4.5\,kV$ . Sample was dissolved in acetonitrile  $(1\,mg\,ml^{-1})$  and was injected in the ion source by an autosampler (Surveyor) with a flow of pure acetonitrile (0.2 ml min<sup>-1</sup>). The Excalibur 1.4 software is used. The powder X-day diffraction (XRD) measurements of polycrystalline samples were performed. The experiments prove the crystallographic space systems and groups of the studied drugs. The XRD patterns were obtained using a Rigaku MiniFlex powder diffraction system, equipped with a horizontal goniometer in the  $\theta/2\theta$  mode. The X-ray source was nickel-filtered K- $\alpha$  emission of copper (1.5405<sub>6</sub> Å). Samples were packed into an aluminum holder using a back-fill procedure and will be scanned over the range of 50–6 degrees  $2\theta$ , at a scan rate of 0.5 degrees  $2\theta$ /min. Using a data acquisition rate of 1 point per second, the scanning parameters equate to a step size of 0.0084 degrees  $2\theta$ . Calibration of each powder pattern will be effected using the characteristic scattering peaks of aluminum at 44.738 and 38.472 degrees  $2\theta$ .

# 2.3. Statistical methods

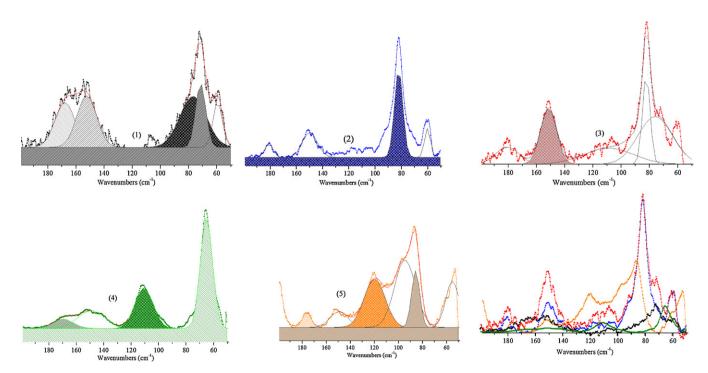
The experimental and theoretical spectroscopic patterns were processed by R4Cal Open Office STATISTICs for Windows 7 [32] program package. Baseline corrections (BLC) and curve-fitting (CF) procedures were applied. The BLC performs operations by multipoint level or function fitting. In the multiple point level method, the baseline was leveled at a value that is the average of the baseline points. The baseline was calculated using the standard linear equation. The CF nonlinear procedure was applied. Although there are many different methods, there is no one perfect one to fit the experimental data-set. In general, non-linear peak fitting methods involve fitting a series of individual functions simultaneously, in order to obtain the single "best fit" solution. The solutions were found by iteratively trying a series of combinations of the parameters until the best one is found. Since the solutions are interdependent, small changes in one of the parameters, affect the final result of all the others. When using an iterative process, the starting point should be as close to the actual solution as possible. Good "guestimates" for the starting values increase the probability of finding the "best" solution. As always no method is perfect, and unfortunately, since there are a number of answers to a non-linear problem, many times the fit will end up in a "local minimum", which may not be the best possible solution. Many fit routines will then continue to iterate using solutions that are significantly different from the minimum, trying to find another "better" solution. If one is not found then the minimized solution is considered "best". Other problems occur if the user input values are significantly far from the "real" answer. This may end in a solution that is stuck in a local minimum that is determined to be the best fit. In extreme cases the fit may even "walk away" to a ridiculous solution. The only way to recover from this problem is to re-enter the starting fit values. Over-fitting is another common problem. Better fits can always be obtained with more input variables (given enough variables you can fit anything). Thus it is important that the input parameters reflect the proper number of variables based on the physical measurement. Using non-linear methods requires a threshold at which the "fit" is considered "good" (i.e. minimizing the merit equation to some near zero value). In the case of the Levenberg-Marquardt method, the merit equation used is  $\chi^2$  the equation. The final solution is found when a minimum in the reduced  $\chi^2$  equation is reached. It is a statistical measure of "goodness-of-fit", inversely proportional to the known variance of the data set. The statistical significance of each regression coefficient was checked by the use of t-test (calculation of the number of significance using data from the experimental error, usually higher than 0.100). The model fit was determined by F-test [33–51]. The most applied smoothing methods for spectroscopic curves interpretation are Savitzky-Golay (SG) and Fourier. Fourier smoothing is based on data inversion by Fast Fourier Transform (FFT) to the time domain, where a trapezoidal filter is applied to the high frequency region. Finally, an inverse FFT is applied to give the smoothed result. The degree of smoothing determines the cut-off point of the filter. A trapezoidal filter is applied to the high frequency region, then inverse FFT to give the smoothed result. The degree or percentage (%) of smoothing determines the cut-off point for the filter. SG smoothing is based on the convolution approach which performs a least-squares fit to a specified part of data points or the procedure is controlled by the level of polynomial and number of points parameters. The degree of polynomial and the number of points are controlled during the procedure by specifies the order of the polynomial to fit over the specified number of points. Thus the larger number of points specified and lower orders of polynomial heavier the smoothing. Only odd numbers are used for number of smoothing points and even values are rounded. The number of smoothing points must be one more than the "degree of polynomial" The algorithm used for generating the SG convolution coefficients has been described. It is worth mentioning that the choice of smoothing parameters is somewhat subjective data-dependent and arbitrary. The (n-1)/2 data points, where n is the number of points used in the convolution function, are truncated from the beginning and end of the procedure.

#### 2.4. Quantitative analysis procedure

For the purpose of the quantitative determination are attributed the integral intensities defined as  $Av_i^{(j,k)}$  at the  $v_i$  frequency for the j- and k-components, common for both the analysed substances in the mixtures to the corresponding value  $Av_i^{(j)}$  for a frequency presented in the corresponding solid-state Raman spectrum of one of the analysed compound. For the isolated compounds and the mixtures, complete separation (deconvolution) of the bands was achieved by employing the 'Peak Fit' statistical procedure, the corresponding baseline method as well as non-linear curve-fitting tools. The peak position and the area under the curve (or  $Av_i^{(j)}$ ) of the separated frequencies were used for the qualitative chemical identification, quantitative determination as well as elucidation of the optical phenomena within the THz-region. The  $Av_i^{(j,k)}$  is directly proportional to the reciprocal mole fraction of one of the compound (1/X). Repeated Raman spectroscopic analysis on three



**Fig. 1.** Smoother solid-state Raman spectra within 200–30 cm<sup>-1</sup> spectroscopic region, using Savitzki–Golay (SG) method and Fast-Fourier Transfer (FFT) filter at different number of points (NP) at left/rigth (L/R) and polynomial orders (PO); the spectroscopic patterns are preliminary procedured by the baseline correction method.



**Fig. 2.** Curve-fitted solid-state Raman spectra within the  $200-30\,\mathrm{cm}^{-1}$ ; curve-fitted spectroscopic patterns after the baseline correction method, by non-linear multipeak Lorenzian–Gaussian function at ratio 1:1; A is the total area under the curve from the baseline centre of the peak;  $w^2$  "sigma", approximately 0.441 the FWHM; w/2 is the standard deviation, respectively.

**Table 1**The experimental peak position  $(v_i^{(j)})$  and integral intensity  $Av_i^{(j)}$  for *i*th-peak at the Raman spectra at of the *j*-compounds **(1)–(5)**, obtained after the smoothing procedures, using Savitzki–Golay (SG) method and Fast-Fourier Transfor (FFT) filter at different number of points (NP) at left/rigth (L/R) and polynomial orders (PO). The obtained average values correspond to the three repeated measurements of the each of the samples.

G-L/R	2/2		6/6		10/10		14/14		18/18		22/22		
	$v_i^{(j)}$	$A\nu_i^{(j)}$	$v_i^{(j)}$	$Av_i^{(j)}$	$v_i^{(j)}$	$Av_i^{(j)}$	$v_i^{(j)}$	$Av_i^{(j)}$	$v_i^{(j)}$	$A\nu_i^{(j)}$	$v_i^{(j)}$	$Av_i^{(j)}$	
20-2													
1 <sup>(1)</sup>	$164.2\pm0.1_2$	$6.111 \pm 0.5_{6}$	$164.1 \pm 0.6_2$	$6.100 \pm 0.5_0$	$164.0 \pm 0.1_{1}$	$6.093 \pm 0.5_2$	$164.0 \pm 0.3_3$	$6.081 \pm 0.2_{1}$	$164.0 \pm 0.1_3$	$6.001 \pm 0.1_{1}$	$164.0 \pm 0.1_1$	$6.000 \pm 0.1_{8}$	(1)
2(1)	$152.3\pm0.3_2$	$6.999\pm0.5_{1}$	$152.5 \pm 0.2_2$	$6.341 \pm 0.2_{1}$	$152.3\pm0.5_{3}$	$6.322\pm0.2_{8}$	$152.2\pm0.2_{1}$	$6.300 \pm 0.2_{2}$	$152.1\pm0.6_{8}$	$6.101 \pm 0.2_2$	$152.1\pm0.6_2$	$6.101 \pm 0.6_2$	
3 <sup>(1)</sup>	$72.3 \pm 0.1_5$	$9.269 \pm 0.1_{7}$	$72.2 \pm 0.1_3$	$9.103 \pm 0.1_3$	$72.1 \pm 0.1_{1}$	$9.088\pm0.1_{1}$	$72.8 \pm 0.1_3$	$9.077 \pm 0.1_{0}$	$72.1 \pm 0.1_2$	$9.077 \pm 0.7_{0}$	$72.1 \pm 0.1_{7}$	$9.075 \pm 0.5_0$	
4 <sup>(1)</sup>	$60.8 \pm 0.1_{6}$	$1.479\pm0.9_{6}$	$60.7\pm0.1_{5}$	$1.444\pm0.9_{5}$	$60.6\pm0.1_4$	$1.112\pm0.6_2$	$60.2\pm0.1_7$	$1.111 \pm 0.5_{1}$	$60.6\pm0.2_3$	$1.001\pm0.1_{8}$	$60.6 \pm 0.2_{1}$	$1.000 \pm 0.9_3$	
1(2)	$181.5\pm0.0_{5}$	$1.221\pm0.5_{1}$	$180.3\pm0.1_{5}$	$1.210 \pm 0.3_{1}$	$181.4 \pm 0.1_3$	$1.209 \pm 0.1_{1}$	$181.5\pm0.5_{4}$	$1.200\pm0.0_{1}$	$181.3 \pm 0.6_{6}$	$1.199\pm0.4_{1}$	$181.2\pm0.1_{6}$	$1.220\pm0.2_{2}$	(2)
(2)	$153.1 \pm 0.3_2$	$4.119 \pm 0.2_{3}$	$153.0\pm0.3_7$	$4.100 \pm 0.2_{0}$	$153.0\pm0.2_{5}$	$4.100\pm0.3_{9}$	$153.1 \pm 0.2_{1}$	$4.075\pm0.1_{3}$	$153.7\pm0.2_{9}$	$4.033\pm0.1_{3}$	$153.1 \pm 0.4_{7}$	$4.103\pm0.1_{8}$	
(2)	$83.5 \pm 0.1_{1}$	$8.152\pm0.2_{8}$	$83.4\pm0.0_1$	$8.103 \pm 0.2_2$	$83.3 \pm 0.6_9$	$8.104 \pm 0.2_{7}$	$83.3 \pm 0.7_{8}$	$8.124 \pm 0.6_{3}$	$83.3\pm0.1_8$	$8.102\pm0.1_{8}$	$83.1 \pm 0.2_{8}$	$8.100 \pm 0.1_4$	
(2)	$61.2 \pm 0.2_2$	$1.967 \pm 0.3_{3}$	$61.1 \pm 0.1_2$	$1.944 \pm 0.1_{8}$	$61.1 \pm 0.1_{8}$	$1.955 \pm 0.3_2$	$61.1 \pm 0.5_{8}$	$1.955 \pm 0.2_{5}$	$61.1 \pm 0.3_3$	$1.955 \pm 0.1_2$	$61.2 \pm 0.1_{1}$	$1.902 \pm 0.0_{1}$	
(3)	$180.3 \pm 0.1_{8}$	$1.141 \pm 0.1_{6}$	$180.3 \pm 0.9_3$	$1.133 \pm 0.1_4$	$180.2 \pm 0.7_4$	$1.120 \pm 0.1_{0}$	$180.2 \pm 0.2_4$	$1.111 \pm 0.1_{1}$	$180.2 \pm 0.3_9$	$1.106 \pm 0.1_{0}$	$180.2 \pm 0.2_4$	$1.101 \pm 0.1_3$	(3)
(3)	$152.7 \pm 0.1_2$	$2.251 \pm 0.3_{8}$	$152.2 \pm 0.1_{1}$	$2.240 \pm 0.2_{2}$	$152.5 \pm 0.5_{1}$	$2.232\pm0.4_{4}$	$152.5 \pm 0.2_3$	$2.227\pm0.5_{5}$	$152.3 \pm 0.3_2$	$2.210 \pm 0.3_{0}$	$152.5 \pm 0.1_{1}$	$2.199 \pm 0.3_{5}$	
(3)	$82.8\pm0.1_6$	$7.166\pm0.3_{4}$	$82.0\pm0.3_{4}$	$7.150 \pm 0.2_{7}$	$82.5 \pm 0.1_3$	$7.155 \pm 0.2_2$	$82.4\pm0.1_0$	$7.140\pm0.2_{3}$	$82.9 \pm 0.1_{0}$	$7.133\pm0.7_{8}$	$82.2\pm0.1_{1}$	$7.127 \pm 0.3_2$	
(4)	$110.3\pm0.5_{8}$	$4.886\pm0.6_2$	$110.2 \pm 0.5_3$	$4.833\pm0.1_{7}$	$110.2 \pm 0.3_2$	$4.813\pm0.2_2$	$110.1 \pm 0.3_1$	$4.810\pm0.6_2$	$110.3\pm0.5_{8}$	$4.808\pm0.1_{4}$	$110.2\pm0.5_{1}$	$4.800\pm0.2_{1}$	(4)
(4)	$64.2\pm0.6_6$	$8.867\pm0.2_{5}$	$64.1 \pm 0.6_{3}$	$8.850 \pm 0.1_{3}$	$64.1 \pm 0.3_2$	$8.842\pm0.1_2$	$64.1 \pm 0.5_5$	$8.807\pm0.2_{5}$	$64.2\pm0.6_6$	$8.800\pm0.1_{2}$	$64.1 \pm 0.6_2$	$8.844\pm0.1_{2}$	
(5)	$177.4 \pm 0.4_3$	$0.993 \pm 0.3_2$	$177.2 \pm 0.1_2$	$0.966 \pm 0.2_{1}$	$177.2 \pm 0.1_{7}$	$0.948 \pm 0.2_{1}$	$177.2 \pm 0.5_2$	$0.953 \pm 0.3_2$	$177.4 \pm 0.4_3$	$0.950 \pm 0.2_{2}$	$177.2 \pm 0.4_2$	$0.949 \pm 0.1_2$	(5)
(5)	$120.1 \pm 0.5_1$	$2.170 \pm 0.5_{5}$	$120.0 \pm 0.5_0$	$2.150 \pm 0.1_{2}$	$120.0 \pm 0.3_3$	$2.133 \pm 0.1_{2}$	$120.0 \pm 0.4_2$	$2.130 \pm 0.5_{5}$	$120.1 \pm 0.5_1$	$2.120 \pm 0.5_{5}$	$120.3 \pm 0.5_2$	$2.118 \pm 0.5_{5}$	
(5)	$87.1 \pm 0.7_{8}$	$7.939\pm0.1_{8}$	$87.0 \pm 0.7_{5}$	$7.933 \pm 0.0_3$	$87.0 \pm 0.6_{6}$	$7.912\pm0.0_{9}$	$87.0 \pm 0.7_{5}$	$7.909 \pm 0.1_{8}$	$87.1 \pm 0.7_{8}$	$7.900 \pm 0.1_{1}$	$87.1 \pm 0.7_{5}$	$7.900 \pm 0.1_{8}$	
G-PO-4													
(1)	$164.2 \pm 0.1_2$	$6.111 \pm 0.4_2$	$164.0 \pm 0.3_2$	$6.092\pm0.5_{1}$	$164.0\pm0.3_{5}$	$6.088\pm0.1_{4}$	$164.0\pm0.6_2$	$6.070 \pm 0.2_{0}$	$164.0 \pm 0.3_{7}$	$6.000 \pm 0.2_{1}$	$164.0\pm0.0_0$	$5.982 \pm 0.1_{3}$	(1)
1)	$152.3 \pm 0.3_1$	$6.999 \pm 0.1_2$	$152.2 \pm 0.2_{1}$	$6.333 \pm 0.2_{0}$	$152.3 \pm 0.5_4$	$6.310 \pm 0.1_{7}$	$152.2 \pm 0.1_3$	$6.289 \pm 0.2_{0}$	$152.1 \pm 0.9_2$	$6.088 \pm 0.3_{2}$	$152.1 \pm 0.2_1$	$5.943 \pm 0.7_{1}$	
1)	$72.3 \pm 0.2_5$	$9.268 \pm 0.1_{2}$	$72.2 \pm 0.1_2$	$9.100 \pm 0.1_{1}$	$72.1 \pm 0.4_{1}$	$9.088 \pm 0.2_{3}$	$72.8 \pm 0.3_{6}$	$9.052 \pm 0.2_{0}$	$72.1 \pm 0.2_{7}$	$9.052 \pm 0.7_{0}$	$72.1 \pm 0.3_5$	$9.011 \pm 0.5_2$	
)	$60.8 \pm 0.1_2$	$1.479 \pm 0.5_{6}$	$60.5 \pm 0.1_2$	$1.411 \pm 0.9_0$	$60.6 \pm 0.2_{3}$	$1.102 \pm 0.5_2$	$60.2 \pm 0.2_{7}$	$1.092 \pm 0.3_{1}$	$60.6 \pm 0.1_9$	$1.000 \pm 0.2_{8}$	$60.6 \pm 0.1_{1}$	$0.993 \pm 0.2_{3}$	
2)	$181.5 \pm 0.0_1$	$1.220 \pm 0.5_{1}$	$180.3 \pm 0.1_{5}$	$1.209 \pm 0.3_{3}$	$181.4 \pm 0.2_{8}$	$1.207 \pm 0.0_{1}$	$181.5 \pm 0.9_{1}$	$1.199 \pm 0.1_{1}$	$181.3 \pm 0.7_{1}$	$1.169 \pm 0.5_0$	$181.2 \pm 0.5_{8}$	$1.218 \pm 0.2_{1}$	(2
2)	$153.1 \pm 0.3_0$	$4.119 \pm 0.2_{2}$	$153.0 \pm 0.1_2$	$4.092 \pm 0.2_{1}$	$153.0 \pm 0.2_9$	$4.099 \pm 0.2_{3}$	$153.1 \pm 0.5_2$	$4.062 \pm 0.3_3$	$153.7 \pm 0.3_5$	$4.024 \pm 0.2_{3}$	$153.1 \pm 0.9_{1}$	$4.077 \pm 0.1_2$	
2)	$83.5 \pm 0.1_{6}$	$8.151 \pm 0.2_{7}$	$83.4 \pm 0.5_3$	$8.096 \pm 0.2_{5}$	$83.3 \pm 0.3_{1}$	$8.100 \pm 0.2_{2}$	$83.3 \pm 0.9_3$	$8.122 \pm 0.6_{3}$	$83.3 \pm 0.9_3$	$8.097 \pm 0.2_{2}$	$83.1 \pm 0.3_1$	$8.042 \pm 0.1_{1}$	
2)	$61.2 \pm 0.2_{1}$	$1.966 \pm 0.3_{2}$	$61.1 \pm 0.2_2$	$1.943 \pm 0.1_{2}$	$61.1 \pm 0.2_3$	$1.933 \pm 0.2_{1}$	$61.1 \pm 0.9_1$	$1.940 \pm 0.2_{4}$	$61.1 \pm 0.3_{7}$	$1.933 \pm 0.2_{2}$	$61.2 \pm 0.7_{6}$	$1.702 \pm 0.0_2$	
3)	$180.3 \pm 0.1_{2}$	$1.140 \pm 0.1_{6}$	$180.3 \pm 0.5_{8}$	$1.142 \pm 0.1_{6}$	$180.3 \pm 0.5_4$	$1.139 \pm 0.1_{5}$	$180.3 \pm 0.7_{2}$	$1.140 \pm 0.1_{5}$	$180.3 \pm 0.2_{9}$	$1.137 \pm 0.1_{5}$	$180.3 \pm 0.9_{6}$	$1.121 \pm 0.1_{7}$	(3)
3)	$152.7 \pm 0.1_{2}$	$2.250 \pm 0.3_{6}$	$152.7 \pm 0.1_{2}$	$2.250 \pm 0.3_{5}$	$152.7 \pm 0.3_{6}$	$2.245 \pm 0.2_{3}$	$152.7 \pm 0.6_{8}$	$2.241 \pm 0.3_{2}$	$152.7 \pm 0.1_{1}$	$2.244 \pm 0.3_{3}$	$152.7 \pm 0.8_{1}$	$2.231 \pm 0.3_{1}$	
(3)	$82.8 \pm 0.1_{1}$	$7.166 \pm 0.3_{3}$	$82.8 \pm 0.1_{2}$	$7.144 \pm 0.1_4$	$82.8 \pm 0.2_{4}$	$7.155 \pm 0.3_{1}$	$82.8 \pm 0.9_2$	$7.150 \pm 0.3_4$	$82.8 \pm 0.1_4$	$7.150 \pm 0.3_{3}$	$82.8 \pm 0.2_{6}$	$7.155 \pm 0.3_{1}$	
4)	$110.3 \pm 0.4_{8}$	$4.885 \pm 0.6_{2}$	$110.3 \pm 0.5_{1}$	$4.877 \pm 0.5_2$	$110.3 \pm 0.1_2$	$4.875 \pm 0.2_{3}$	$110.3 \pm 0.8_{3}$	$4.879 \pm 0.5_{1}$	$110.3 \pm 0.5_{1}$	$4.877 \pm 0.4_{2}$	$110.3 \pm 0.5_{1}$	$4.865 \pm 0.2_{2}$	(4
(4)	$64.2 \pm 0.5_{5}$	$8.868 \pm 0.2_{5}$	$64.2 \pm 0.7_{8}$	$8.851 \pm 0.2_{1}$	$64.2 \pm 0.6_{8}$	$8.866 \pm 0.1_{5}$	$64.2 \pm 0.7_{8}$	$8.860 \pm 0.2_{1}$	$64.2 \pm 0.1_{7}$	$8.859 \pm 0.2_{1}$	$64.2 \pm 0.6_2$	$8.839 \pm 0.2_{1}$	
(5)	$177.4 \pm 0.5_2$	$0.992 \pm 0.3_{2}$	$177.4 \pm 0.5_{1}$	$0.966 \pm 0.3_{1}$	$177.4 \pm 0.7_{7}$	$0.991 \pm 0.3_{1}$	$177.4 \pm 0.4_2$	$0.990 \pm 0.3_{3}$	$177.4 \pm 0.5_2$	$0.977 \pm 0.2_{2}$	$177.4 \pm 0.5_{3}$	$0.982 \pm 0.2_{2}$	(5)
5)	$120.1 \pm 0.5_{1}$	$2.171 \pm 0.5_{1}$	$120.1 \pm 0.2_2$	$2.169 \pm 0.1_{1}$	$120.1 \pm 0.5_9$	$2.166 \pm 0.5_{0}$	$120.1 \pm 0.5_0$	$2.163 \pm 0.5_{1}$	$120.1 \pm 0.5_{5}$	$2.169 \pm 0.5_{2}$	$120.1 \pm 0.5_{7}$	$2.179 \pm 0.1_{5}$	
5)	$87.1 \pm 0.7_{1}$	$7.938 \pm 0.1_{3}$	$87.1 \pm 0.9_2$	$7.928 \pm 0.1_{2}$	$87.1 \pm 0.6_{3}$	$7.925 \pm 0.1_{1}$	$87.1 \pm 0.7_{1}$	$7.933 \pm 0.1_{2}$	$87.1 \pm 0.8_{8}$	$7.955 \pm 0.1_{1}$	$87.1 \pm 0.8_{8}$	$7.918 \pm 0.1_{2}$	
G-PO-6													
(1)	$164.2 \pm 0.2_{1}$	$6.110 \pm 0.5_3$	$164.1 \pm 0.4_3$	$6.097 \pm 0.2_{0}$	$164.0 \pm 0.1_5$	$6.001 \pm 0.5_2$	$164.0 \pm 0.1_3$	$6.055 \pm 0.2_2$	$164.0 \pm 0.1_{1}$	$5.997 \pm 0.2_{1}$	$164.0 \pm 0.1_2$	$5.994 \pm 0.2_{8}$	(1
(1)	$152.3 \pm 0.1_2$	$6.977 \pm 0.5_{0}$	$152.5 \pm 0.3_2$	$6.322 \pm 0.2_{1}$	$152.3 \pm 0.5_{1}$	$6.112 \pm 0.2_3$	$152.2 \pm 0.1_{7}$	$6.220 \pm 0.2_{1}$	$152.1 \pm 0.6_2$	$6.055 \pm 0.2_2$	$152.1 \pm 0.6_3$	$6.000 \pm 0.5_2$	
(1)	$72.3 \pm 0.1_2$	$9.267 \pm 0.1_{8}$	$72.2 \pm 0.1_{8}$	$9.100 \pm 0.1_{1}$	$72.1 \pm 0.2_3$	$9.025 \pm 0.1_{7}$	$72.8 \pm 0.9_2$	$9.068 \pm 0.0_{0}$	$72.1 \pm 0.1_2$	$9.031 \pm 0.6_{0}$	$72.1 \pm 0.1_2$	$9.055 \pm 0.3_{0}$	
1)	$60.8 \pm 0.12_{6}$	$1.478 \pm 0.9_{2}$	$60.7 \pm 0.1_9$	$1.427 \pm 0.3_{5}$	$60.6 \pm 0.3_4$	$1.102 \pm 0.6_{3}$	$60.2 \pm \pm 0.3_{5}$	$1.100 \pm 0.5_{5}$	$60.6 \pm 0.2_{3}$	$1.000 \pm 0.1_{2}$	$60.6 \pm 0.2_{7}$	$0.971 \pm 0.8_{3}$	
(2)	$181.5 \pm 0.1_5$	$1.220 \pm 0.3_{1}$	$180.3 \pm 0.2_{5}$	$1.201 \pm 0.1_{1}$	$181.4 \pm 0.1_1$	$1.200 \pm 0.1_{0}$	$181.5 \pm 0.5_1$	$1.177 \pm 0.2_{1}$	$181.3 \pm 0.6_{1}$	$1.177 \pm 0.6_{1}$	$181.2 \pm 0.3_{6}$	$1.188 \pm 0.2_{2}$	(2)
(2)	$153.1 \pm 0.2_{2}$	$4.118 \pm 0.1_{3}$	$153.0 \pm 0.8_{7}$	$3.999 \pm 0.1_{0}$	$153.0 \pm 0.8_2$	$4.100 \pm 0.3_{2}$	$153.1 \pm 0.2_{0}$	$4.043 \pm 0.1_2$	$153.7 \pm 0.3_{1}$	$4.021 \pm 0.1_3$	$153.1 \pm 0.4_{1}$	$4.001 \pm 0.2_{8}$	
(2)	$83.5 \pm 0.2_{1}$	$8.151 \pm 0.2_{1}$	$83.4\pm0.0_8$	$8.103 \pm 0.2_{2}$	$83.3 \pm 0.9_{1}$	$8.100 \pm 0.2_{1}$	$83.3 \pm 0.7_{1}$	$8.115 \pm 0.6_{3}$	$83.3 \pm 0.2_{3}$	$8.005 \pm 0.1_9$	$83.1 \pm 0.3_2$	$8.093 \pm 0.4_4$	
(2)	$61.2 \pm 0.2_{1}$	$1.968 \pm 0.3_{3}$	$61.1 \pm 0.1_9$	$1.944 \pm 0.1_{8}$	$61.1 \pm 0.3_2$	$1.913 \pm 0.3_2$	$61.1 \pm 0.6_2$	$1.944 \pm 0.2_{1}$	$61.1 \pm 0.1_{8}$	$1.933 \pm 0.1_{1}$	$61.2 \pm 0.1_3$	$1.900 \pm 0.0_0$	
(3)	$180.3 \pm 0.1_{1}$	$1.140 \pm 0.1_{6}$	$180.3 \pm 0.2_{8}$	$1.141 \pm 0.1_{6}$	$180.3 \pm 0.9_{1}$	$1.128 \pm 0.1_{3}$	$180.3 \pm 0.8_{1}$	$1.135 \pm 0.1_{7}$	$180.3 \pm 0.9_{1}$	$1.127 \pm 0.1_{2}$	$180.3 \pm 0.7_{1}$	$1.133 \pm 0.1_{2}$	(3)
(3)	$152.7 \pm 0.1_2$	$2.250 \pm 0.3_{8}$	$152.7 \pm 0.1_{7}$	$2.251 \pm 0.3_{8}$	$152.7 \pm 0.5_2$	$2.244 \pm 0.3_{5}$	$152.7 \pm 0.9_2$	$2.250 \pm 0.3_{1}$	$152.7 \pm 0.3_{1}$	$2.227 \pm 0.3_{1}$	$152.7 \pm 0.1_{2}$	$2.250 \pm 0.3_{3}$	
(3)	$82.8 \pm 0.1_{2}$	$7.161 \pm 0.3_4$	$82.8 \pm 0.2_{7}$	$7.166 \pm 0.3_4$	$82.8 \pm 0.7_{1}$	$7.155 \pm 0.3_{1}$	$82.8 \pm 0.1_{2}$	$7.144 \pm 0.3_4$	$82.8 \pm 0.7_{1}$	$7.144 \pm 0.3_{1}$	$82.8 \pm 0.3_{6}$	$7.152 \pm 0.3_{5}$	
(4)	$110.3 \pm 0.5_{6}$	$4.885 \pm 0.6_{2}$	$110.3 \pm 0.1_{9}$	$4.886 \pm \pm 0.6_{2}$	$110.3 \pm 0.9_{1}$	$4.833 \pm 0.6_{2}$	$110.3 \pm 0.4_{1}$	$4.871 \pm 0.6_{1}$	$110.3 \pm 0.5_{8}$	$4.873 \pm 0.6_{1}$	$110.3 \pm 0.1_{8}$	$4.866 \pm 0.5_{3}$	(4)
(4)	$64.2 \pm 0.6_{8}$	$8.866 \pm 0.2_{5}$	$64.2 \pm 0.5_{8}$	$8.867 \pm 0.2_{5}$	$64.2 \pm 0.7_{1}$	$8.855 \pm 0.2_{1}$	$64.2 \pm 0.2_{6}$	$8.832 \pm 0.2_{1}$	$64.2 \pm 0.6_{5}$	$8.882 \pm 0.1_{5}$	$64.2 \pm 0.6_{6}$	$8.893 \pm 0.2_{1}$	
(5)	$177.4 \pm 0.4_9$	$0.992 \pm 0.3_{1}$	$177.4 \pm 0.2_{3}$	$0.993 \pm \pm 0.3_2$	$177.4 \pm 0.7_{1}$	$0.918 \pm 0.3_{1}$	$177.4 \pm 0.4_{1}$	$0.919 \pm 0.1_{2}$	$177.4 \pm 0.5_{5}$	$0.944 \pm 0.2_{2}$	$177.4 \pm 0.6_{3}$	$0.933 \pm 0.4_{1}$	(5)
(5)	$120.1 \pm 0.5_3$	$2.171 \pm 0.5_{5}$	$120.1 \pm 0.1_1$	$2.170 \pm 0.5_{5}$	$120.1 \pm 0.9_1$	$2.155 \pm 0.5_{1}$	$120.1 \pm 0.5_0$	$2.152 \pm 0.1_{5}$	$120.1 \pm 0.5_5$	$2.166 \pm 0.1_{5}$	$120.1 \pm 0.5_7$	$2.149 \pm 0.1_9$	()
(5)	$87.1 \pm 0.7_{2}$	$7.937 \pm 0.1_{8}$	$87.1 \pm 0.7_{9}$	$7.939 \pm \pm 0.1_{8}$	$87.1 \pm 0.9_{8}$	$7.927 \pm 0.1_{1}$	$87.1 \pm 0.7_3$	$7.929 \pm 0.2_{8}$	$87.1 \pm 0.7_{5}$	$7.919 \pm 0.2_{8}$	$87.1 \pm 0.7_{9}$	$7.911 \pm 0.2_{7}$	

(======================================	(5.55)												
SG-L/R	2/2		9/9		10/10		14/14		18/18		22/22		
	$\nu_i^{(j)}$	$A\nu_i^{(j)}$	$\mathbb{Q}_i^{\mathcal{N}}$	$A\nu_i^{(j)}$	V <sub>i</sub> (i)	$A \nu_i^{(j)}$	$\nu_i^{(j)}$	$A\nu_i^{(j)}$	ν <sub>i</sub>	$A\nu_i^{(j)}$	ν <sub>i</sub> (θ)	$A \nu_i^{(j)}$	
FFT-NP	3		5		7		6						
$\nu_1^{(1)}$	$164.2\pm0.2_2$	$6.110\pm0.5_2$	$164.1\pm0.6_3$	$6.057 \pm 0.5_{1}$	$164.0\pm0.2_{1}$	$6.064 \pm 0.5_1$	$164.0\pm0.2_{\rm 2}$	$6.033 \pm 0.2_{3}$					(1)
$\nu_{2}^{(1)}$	$152.3 \pm 0.4_2$	$6.986 \pm 0.5_{0}$	$152.5 \pm 0.3_3$	$6.243\pm0.1_{1}$	$152.3 \pm 0.2_3$	$6.310 \pm 0.2_1$	$152.2\pm0.1_7$	$6.271\pm0.1_2$					
$\nu_{3}^{(1)}$	$72.3\pm0.2_5$	$9.266 \pm 0.1_{2}$	$72.2\pm0.3_9$	$9.005\pm0.0_2$	$72.1\pm0.3_1$	$9.073\pm0.1_{9}$	$72.8\pm0.6_1$	$9.034\pm0.2_0$					
$\nu_{4}^{(1)}$	$60.8\pm0.2_{6}$	$1.475 \pm 0.9_1$	$60.7\pm0.4_7$	$1.430\pm0.8_8$	$60.3\pm0.1_8$	$1.018\pm0.6_2$	$60.2\pm0.8_2$	$1.056\pm0.5_2$					
$\nu_1^{(2)}$	$181.5 \pm 0.0_2$	$1.220 \pm 0.5_0$	$180.3\pm0.8_2$	$1.200\pm0.2_1$	$181.4 \pm 0.9_3$	$1.200 \pm 0.2_1$	$181.5 \pm 0.7_2$	$1.188\pm0.1_1$					(2)
$\nu_{2}^{(2)}$	$153.1\pm0.1_2$	$4.117\pm0.1_2$	$153.0\pm0.47$	$4.082\pm0.2_0$	$153.0 \pm 0.9_1$	$4.092 \pm 0.3_1$	$153.1\pm0.9_1$	$4.055 \pm 0.3_3$					
$\nu_{3}^{(2)}$	$83.5\pm0.1_8$	$8.151\pm0.2_4$	$83.4\pm0.5_1$	$8.033 \pm 0.3_2$	$83.3 \pm 0.7_2$	$8.087\pm0.2_2$	$83.3\pm0.8_9$	$8.115 \pm 0.3_3$					
$\nu_{4}^{(2)}$	$61.2\pm0.2_2$	$1.965 \pm 0.3_1$	$61.1\pm0.8_2$	$1.930\pm0.1_{8}$	$61.1\pm0.3_1$	$1.933 \pm 0.3_1$	$61.1\pm0.5_1$	$1.905\pm0.1_{5}$					
$\nu_1^{(3)}$	$180.3\pm0.1_8$	$1.141\pm0.1_{6}$	$180.3\pm0.9_2$	$1.140\pm0.2_3$	$180.3\pm0.9_2$	$1.128\pm0.1_2$	$180.3\pm0.5_8$	$1.139\pm0.2_{6}$					(3)
$\nu_{2}^{(3)}$	$152.7\pm0.1_4$	$2.250 \pm 0.3_{6}$	$152.7\pm0.8_2$	$2.250\pm0.5_2$	$152.7\pm0.1_8$	$2.242 \pm 0.3_3$	$152.7 \pm 0.5_2$	$2.222 \pm 0.1_8$					
$\nu_{3}^{(3)}$	$82.8\pm0.1_2$	$7.165 \pm 0.3_5$	$82.8\pm0.7_6$	$7.122\pm0.8_{9}$	$82.8\pm0.9_1$	$7.155 \pm 0.3_2$	$82.8\pm0.4_4$	$7.155\pm0.1_{4}$					
$\nu_{1}^{(4)}$	$110.3 \pm 0.5_2$	$4.885 \pm 0.6_{1}$	$110.3 \pm 0.6_8$	$4.877\pm0.5_2$	$110.3 \pm 0.9_1$	$4.877\pm0.6_2$	$110.3\pm0.1_8$	$4.816\pm0.1_2$					(4)
$\nu_{2}^{(4)}$	$64.2\pm0.6_1$	$8.864 \pm 0.2_1$	$64.2\pm0.5_{6}$	$8.854\pm0.1_{5}$	$64.2\pm0.6_1$	$8.855 \pm 0.2_{1}$	$64.2\pm0.5_5$	$8.855\pm0.1_{5}$					
$\nu_{1}^{(5)}$	$177.4\pm0.4_8$	$0.991\pm0.1_2$	$177.4\pm0.1_3$	$0.922\pm0.2_2$	$177.4 \pm 0.5_9$	$0.955 \pm 0.3_{1}$	$177.4 \pm 0.5_3$	$0.977 \pm 0.3_3$					(5)
$\nu_{2}^{(5)}$	$120.1\pm0.4_1$	$2.169\pm0.2_5$	$120.1\pm0.2_1$	$2.169\pm0.8_5$	$120.1\pm0.5_9$	$2.156\pm0.5_1$	$120.1\pm0.1_1$	$2.161\pm0.1_{5}$					
$\nu_{3}^{(5)}$	$87.1\pm0.6_8$	$7.929\pm0.1_1$	$87.1\pm0.2_8$	$7.929 \pm 0.1_8$	$87.1\pm0.7_{\rm 0}$	$7.929\pm0.1_8$	$87.1\pm0.7_{\rm 1}$	$7.927\pm0.1_7$					

replicate samples for each mole fraction was applied as well as the measurements is repeated three times. The results of mean value for area ratio of the peaks together with between assay precision data (RSD%) are presented. Regression analysis of the data gave a straight-line calibration plot with confidence intervals for slope and intercept, are defined. The validity of the obtained equations is confirmed from the spectrum of the pure substances where the corresponding  $Av_i^{(j)}/Av_i^{(k)}$  values are obtained. The  $Av_i^{(j)}$  measured in the Raman spectrum depends on the intensity of the laser  $I_0$ , on a factor  $K(v_i)$  including the frequency dependent terms (such as overall spectrophotometer response, self-absorption of the medium and molecular scattering of the Raman active species), and on the mole fraction (X) of the active species. Therefore, for two component mixtures, the equations are:

$$\begin{split} A\nu_i^{(j)} &= I_0 K(\nu_i^{(j)}) X \\ &\text{Therefore,} \\ K^{(j)} \nu_i^{(j,k)} X. \end{split} \qquad A\nu_i^{(j,k)} / A\nu_i^{(j)} &= [K^{(j)} \nu_i^{(j,k)} X + K^{(k)} \nu_i^{(k)} (1-X)] / K^{(j)} \nu_i^{(j,k)} X. \end{split}$$

# 2.5. Multiple linear regression (MLR)

To perform a MLR analysis on the data, highlight the independent variable columns of data sets. The first group contains the dependent variable values, Y, and the highlighted columns assumed to contain the independent variables, X. The common statement consists of that the dependent data,  $y_i$ , depends linearly on several independent variables,  $x_1, x_2, ..., x_k$  as well as that the given data depends only on two independent variables. The data sets could be written as  $(x_{11}, x_{21}, y_1)$ ,  $(x_{12}, x_{22}, y_2)$ ,  $(x_{13}, x_{23}, y_3)$ , ...,  $(x_{1N}, x_{2N}, y_N)$ , respectively. The main aim is to minimize the sum:

$$R^{2} = \sum_{i=1}^{N} (a_{1}x_{1i} + a_{2}x_{2i} + b - y_{i})^{2}$$

The corresponding coefficients  $a_0$ ,  $a_1$ ,  $a_2$  so are found by the following equations:

$$a_1x_{11} + a_2x_{21} + b = y_1$$
  
 $a_1x_{12} + a_2x_{22} + b = y_2$   
 $a_1x_{13} + a_2x_{23} + b = y_3$   
...  
 $a_1x_{1N} + a_2x_{2N} + b = y_N$ 

In matrix form the following presentation is valid:  $A \cdot W = Y$ 

$$A = \begin{pmatrix} x_{11} & x_{21} & 1 \\ x_{12} & x_{22} & 1 \\ x_{1N} & x_{2N} & 1 \end{pmatrix}; \qquad W = \begin{pmatrix} a_1 \\ a_2 \\ b \end{pmatrix} \quad \text{and} \quad Y = \begin{pmatrix} y_1 \\ y_2 \\ y_N \end{pmatrix}$$

The solution of this predetermined system is  $W = (A^t A)^{-1} A^t Y$ 

The obtained values are respectively, t-value: The t-values for testing if the parameter equals zero, where t = the parameter estimate/standard error of the estimate; p-value: The corresponding p-values. A partial F-test is computed for each of the independent variables still in the equation. F statistic = [RSS² – RSS¹]/ESD², where RSS¹ = the residual sum of squares with all variables that are presently in the equation; RSS² = the residual sum of squares with one of the variables removed, and ESD¹ = the Mean Square for Error with all variables that are presently in the equation [52–54].

# 2.6. Analysis of variance (ANOVA) for MLR

The ANOVA test includes Levene's test and the Brown–Forsythe test for equal variance. It is preformed to test whether or not two or

**Table 2** Solid-state Raman frequencies and assignment of the studied compounds within 200–30 cm<sup>-1</sup>;  $\nu$  [cm<sup>-1</sup> (THz)].

	(1)	(2)	(3)	(4)	(5)
H-bonding deformations NH···O(SO), NH···N <sub>Pv</sub>		181 (5.43)	180 (5.4)	170 (5.1)	177 (5.3 <sub>1</sub> )
, , , , , ,	164 (4.92)				
	152 (4.5 <sub>6</sub> )	153 (4.59)	157 (4.7 <sub>1</sub> )	157 (4.7 <sub>1</sub> )/144 (4.3 <sub>2</sub> )	153 (4.59)
					120 (3.6)
		111 (3.3 <sub>3</sub> )	110 (3.3)	110 (3.3)	
Skeletal modes	103 (3.0 <sub>9</sub> )				98 (2.9 <sub>4</sub> )
		83 (2.4 <sub>9</sub> )	85 (2.5 <sub>5</sub> )		87 (2.6 <sub>1</sub> )
	72 (2.1 <sub>6</sub> )		71 (2.1 <sub>3</sub> )		
	60 (1.8)	61 (1.8 <sub>3</sub> )	62 (1.8 <sub>6</sub> )	64 (1.9 <sub>2</sub> )	60 (1.8)
Torsion of entire side chain about the aromatic system					55 (1.6 <sub>5</sub> )

**Table 3** Student's *t*-test data for the smoothed by Savitzky–Golay and Fourier methods; *N* = 16.

SG-L/R					SG-L/R				
PO-2	r	r <sup>2</sup>	SD	p	PO-4	r	$r^2$	SD	р
2/2-6/6	0.99412	0.98827	0.533	<0.0001	2/2-6/6	0.99221	0.98249	0.667	<0.0001
2/2-10/10	$0.9911_{2}$	$0.9823_{1}$	0.432	0.0421	2/2-10/10	0.98312	$0.9665_2$	0.731	0.2521
2/2-22/22	0.99013	0.9803 <sub>5</sub>	0.762	0.0720	2/2-22/22	0.9901	$0.9802_9$	0.785	0.1217
SG-L/R					SG-FFT				
PO-6	r	r <sup>2</sup>	SD	p		r	$r^2$	SD	p
2/2-6/6 2/2-10/10 2/2-22/22	0.9921 <sub>1</sub> 0.9909 <sub>3</sub> 0.9902 <sub>1</sub>	0.9842 <sub>8</sub> 0.9819 <sub>4</sub> 0.9805 <sub>1</sub>	0.531 0.312 0.352	<0.0001 0.0121 0.0220	PO-2 L/R 10/10, NP-3	0.9998	0.9996	0.427	<0.0001

**Table 4** The straight-line plot from the regression analysis of the *n*-component mixtures;  $y = A + B \cdot x$ ; N = 10.

	Α	В	SD	$r^2$	p
(3)/(4)	$11.0 \pm 0.034$	$-1.0 \pm 0.21$	0.003	0.99989	<0.0001
(2)/(5)	$2.905 \pm 0.066$	$-0.174 \pm 0.21$	0.088	$0.9876_2$	< 0.0001
(1)/(4)	$1.789 \pm 0.071$	$-0.095 \pm 0.011$	0.105	0.9461	< 0.0001
(2)/(3)/(4)-(4)	$3.069 \pm 0.038$	$-0.121 \pm 0.006$	0.057	$0.9894_2$	< 0.0001
(2)/(3)/(4)-(3)	$1.913 \pm 0.405$	$1.493 \pm 0.065$	0.593	$0.9924_{3}$	< 0.0001
(1)/(3)/(4)/(5)-(3)	$0.516 \pm 0.005$	$0.024 \pm 0.000$	0.008	$0.9949_1$	< 0.0001
(1)/(2)/(3)/(4)-(3)/(2)	$0.883 \pm 0.011$	$0.038 \pm 0.002$	0.016	0.99175	< 0.0001
(1)/(2)/(3)/(4)/(5)-(3)/(2)	$0.939 \pm 0.014$	$-0.041\pm0.002$	0.0204	0.98843	< 0.0001
(1)/(2)/(3)/(4)/(5)-(5)	$14.141 \pm 0.135$	$-1.103 \pm 0.022$	0.198	0.99844	< 0.0001

more populations have the same mean. The main analysis is based on the assumption that the data sets have been drawn from populations that follow a normal distribution with constant variance. The null hypothesis is that the means of all selected data sets are equal. The alternative hypothesis is that the means of one or more selected data sets are different [55,56].

The basic equations for the ANOVA calculations are:

$$(y_i - \bar{y}) = (\hat{y}_i - \bar{y}) + (y_i - \hat{y}_i)$$

The first term is the total variation, while the second term is the variation in mean response. The third term is the residual value. The equation may also be written as SST=SSM+SSE, where SS is notation for sum of squares and T, M, and E are notation for total, model, and error, respectively. The square of the sample correlation is equal to the ratio of the model sum of squares to the total sum of squares:  $r^2 = SSM/SST$ . The interpretation of  $r^2$  is to explain the fraction of variability in the data explained by the regression model. The sample variance  $s_v^2$  is equal to:

$$s_y^2 = \frac{\sum_i (y_i - \bar{y})^2}{(n-1)}$$

Last equation is the total sum of squares divided by the total degrees of freedom (df). For simple linear regression, the MSM (mean square model) is given by:

$$MSM = \sum_{i} (\hat{y}_i - \bar{y})^2 = \frac{SSM}{DFM}$$

The above is since the simple linear regression model has one explanatory variable x.

The corresponding MSE (mean square error) values are obtained by:

$$MSE = \frac{\sum_{i} (y_i - \hat{y}_i)^2}{(n-2)} = \frac{SSE}{DFE}, \text{ respectively.}$$

#### 3. Results and discussion

3.1. Limits of detection (LODs), smoothing procedure validation, accuracy, precision and assignment of the solid-state Raman spectra within THz-region

The solid-state Raman spectra of the studied compound (1)–(5) are depicted in Figs. 1 and 2. The spectroscopic patterns are

**Table 5** Multiple regression analysis and ANOVA test the data in Table 1 for the  $v_i^{(j)}$  and  $Av_i^{(j)}$ ; the Prob. F value for all calculations is <0.0001.

	Value	Std. Error	t-Value	Prob (>  <i>t</i>  )	$r^2$	ESD		df	SS	MS	F Statistic	
2.28 10-10	SG-L/R 2/2, PO =	= 2 vs. FFT/NP = 3										$\nu_{\cdot}^{(j)}$
1	, , ,	,		$0.9999_1$	1	$3.4\times10^{-9}$	Model	2	32102.1375	16051.0687 <sub>5</sub>	$1.4\times10^{-21}$	1
SC-LIR (SR, PO - 2 xr, FFT)  PO - 1	1	$2.6\times10^{-9}$	$3.8\times10^8$	< 0.0001			Error	13	$1.5\times10^{-16}$	$1.5\times10^{-17}$		
0.1566	$2.1\times10^{-12}$	$2.6\times10^{-9}$	$7.9\times10^{-9}$	$0.9993_{8}$			Total	15	32102.1375			
0.0050   0.004	SG-L/R 6/6, PO =	= 2 vs. FFT/NP = 5										
1949   1949		-		-	1	0.0745	Model	2			$2.8 \times 10^{-6}$	
SC-LIPE   1010	-									0.00555		
0.00146, 0.0145, 0.0145, 0.0145, 0.0145, 0.0145, 0.0145, 0.0146, 0.0	-		_	< 0.0001			Total	15	32102.1375			
0.8446												
0.14876					$0.99999_9$	0.1288					967544.21937	
SC-LIR 21, PO - 4"										0.01659		
-1   -1   -1   -1   -1   -1   -1   -1	_			0.22137			TOLAI	15	32102.1373			
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	, , ,	,		0 99939	1	2 12335F_9	Model	2	32102 1375	16051 06875	$3.6 \times 10^{21}$	
14   10   1   1930  1930  195   70   70   70   70   70   70   70   7					1	2.12333L-3					3.0 × 10	
Sc.LIR, Sc. No. Pol-First Property   Sc.LIR, Sc. No. Pol-First Property   Sc.LIR, Sc. No. Pol-First Property   Sc.LIR, Sc.LI										4.50005E-10		
0.1315   0.06701   1.96255   0.07146   0.09042   0.09042   0.0816   2   0.2020312   0.0816				0.555 15			Total	13	32102.1373			
	, , ,	,		0.07146	1	0.09042	Model	2	32102.03122	16051.01561	$1.9 \times 10^6$	
1.0269												
0.00900	_									· ·		
0.94422	SG-L/R 10/10, P	O = 4 vs. FFT/NP =	= 7									
0.0547    0.1958	$0.2030_{7}$	$0.0994_2$	$2.0425_1$	$0.0619_3$	$0.99999_9$	$0.1363_2$	Model	2	32101.8959 <sub>2</sub>	16050.9479 <sub>6</sub>	863735.22404	
	$0.9442_{3}$	$0.1956_{7}$	4.82559	$3.3  imes 10^{-4}$			Error	13	0.24158	0.01858		
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	0.05477	0.1958	$0.2797_{5}$	$0.7840_{7}$			Total	15	32102.1375			
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $												
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $				-	1	$1.5 \times 10^{-9}$	Model				$7.5 \times 10^{21}$	
Sc-UR   21/2   PO = V   SC-UR   21/2   PO = V   0.0001										$2.1 \times 10^{-18}$		
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $				0.98677			Total	15	32102.1375			
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $											21	
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $					1	$1.4 \times 10^{-9}$					$6.9 \times 10^{21}$	
										$2.1 \times 10^{-18}$		
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $			_	0.99422			Total	13	28507.8035 <sub>7</sub>			
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $				0.0514	1	0.0022	Model	2	20507 7272	14252 9626	21106	
0.06954		_	-		1	0.06327			-		2.1 × 10	
SC-L R   10/10, PO-6 vs. ScI-L R   10/10, PO-6 vs. ScI-R R   10/1				-						0.0003		
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				10.0001			Total	15	20307.00337			
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $				0.00373	1	0.06681	Model	2	28507.75447	14253.87724	$3.2 \times 10^{6}$	
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $					-							
$ \begin{aligned} &   SC-L R \ 14 14,   PO=6 \ vs. \ SC-L R \ 14 14,   PO=4 \ 0.1570_1 & 0.1136 & 1.3821_2 & 0.1902_2 & 0.9999_9 & 0.1601_1 & Model & 2 & 32101.8042_3 & 1605.9021_2 & 626109.4948 \\ & 0.4230_9 & 0.1431_5 & 2.9556_6 & 0.0111_5 & & & & & & & & & & & & & & & & & & &$	-											
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	SG-L/R 14/14, P		14/14, PO = 4						•			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$0.1570_{1}$	0.1136	1.38212	$0.1902_2$	$0.99999_9$	0.16011	Model	2	32101.8042 <sub>3</sub>	16050.9021 <sub>2</sub>	626109.4948	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$0.4230_9$	0.14315	$2.9556_{6}$	$0.0111_{5}$			Error	11	$0.3332_{7}$	$0.0256_{4}$		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0.57627	$0.1430_9$	$4.0274_1$	$0.0014_{4}$			Total	13	32102.1375			
1.01539	SG-L/R 2/2, PO =	= 2 vs. FFT/NP = 3										$Av_i^{(j)}$
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$8.9 \times 10^{-4}$	$0.0011_{7}$	$0.7544_{7}$	$0.4640_2$	1	$0.0025_{3}$	Model	2			$1.110^{7}$	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1.0153 <sub>9</sub>	$0.0042_4$					Error			$6.410^{-6}$		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	-		_	0.0037			Total	15	143.1173 <sub>1</sub>			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		,										
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$					$0.9968_2$	0.1871 <sub>5</sub>					2036.6187 <sub>1</sub>	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$										$0.0350_2$		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				0.3581 <sub>7</sub>			Total	15	143.1173 <sub>1</sub>			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		,		0.4400	0.0000	0.1001	3.4 - 4 - 1	2	1.40.0007	71 2222	2050 2050	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			_	-	0.99685	0.18616				-	2058.2859 <sub>5</sub>	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-	•	-							0.03466		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$				0.09308			TOLAI	15	143.11/31			
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		,		0.6074	0.0076	0.150//	Model	2	142 7867-	71 3033-	2807 7601.	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-			-	0.33709	0.13346					2007.70914	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	-	-								0.02343		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	-	-	3.10033	0.00004			. 5001	1.3				
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		,	0.25106	0.8056a	1	0.00254	Model	2	143.12905	71.56453	$1.1 \times 10^7$	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				-							· -	
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$										-		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			-	-					•			
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		,	0.28728	$0.7784_{3}$	$0.9966_9$	$0.1908_{5}$	Model	2	142.6556 <sub>5</sub>	71.32782	1958.3438 <sub>5</sub>	
SG-L/R 10/10, PO = 4 vs. FFT/NP = 7  0.06477	$0.6634_{7}$	0.57957	1.1447 <sub>5</sub>	0.27295			Error	13	0.47349	$0.0364_2$		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$0.3506_{6}$	$0.5725_2$	$0.6124_9$	0.55078			Total	15	143.12914			
$-0.1467_2$ 2.2908 $-0.0640_5$ 0.9499 <sub>1</sub> Error 13 0.5538 <sub>5</sub> 0.0426		O = 4  vs.  FFT/NP =	= 7									
	-				$0.9961_3$	$0.2064_1$					1673.26148	
$1.1534$ $2.2975_8$ $0.5020_1$ $0.6240_6$ Total $15$ $143.1291_4$			-							0.0426		
	1.1534	2.2975 <sub>8</sub>	0.5020 <sub>1</sub>	$0.6240_{6}$			Total	15	143.1291 <sub>4</sub>			

Table 5 (Continued)

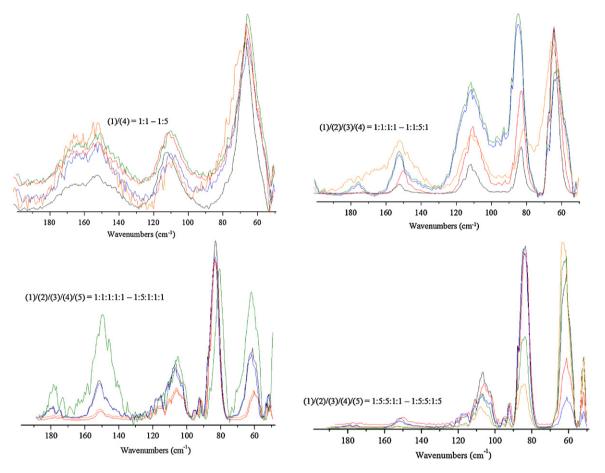
Value	Std. Error	t-Value	Prob $(> t )$	r <sup>2</sup>	ESD		df	SS	MS	F Statistic
SG-L/R 14/14, F	PO = 4 vs. FFT/NF	P=9				<u> </u>		·	·	
$0.0648_2$	$0.0544_9$	1.18969	$0.2554_4$	$0.9987_2$	$0.1185_{6}$	Model	2	142.9464 <sub>1</sub>	$71.4732_1$	5085.0052 <sub>9</sub>
4.01133	4.01133	7.06228	<0.0001			Error	13	0.18272	$0.0140_{6}$	
$-3.0080_1$	$0.5682_{8}$	$-5.2931_{6}$	$1.5 \times 10^{-5}$			Total	15	143.12914		
SG-L/R 2/2, PO	= 6 vs. FFT/NP =	3								
$9.1 \times 10^{-4}$	$0.0012_{7}$	$0.7129_1$	0.4884	1	$0.0027_{5}$	Model	2	142.96334	71.48167	$9.5 \times 10^{6}$
$0.9849_{7}$	$0.0043_{7}$	225.1492 <sub>4</sub>	< 0.0001			Error	13	$9.8 \times 10^{-5}$	$7.6\times10^{-6}$	
$0.0151_{4}$	$0.0044_{3}$	3.4151 <sub>7</sub>	$0.0046_{1}$			Total	15	142.9634 <sub>3</sub>		
SG-L/R 6/6, PO	= 6 vs. FFT/NP =	5								
$-0.0429_2$	$0.0899_{7}$	$-0.4770_{6}$	$0.6412_4$	0.99718	$0.1761_2$	Model	2	142.5602 <sub>1</sub>	71.2801	2298.0647 <sub>9</sub>
1.74895	$0.5332_{6}$	3.27974	$0.0059_{8}$			Error	13	$0.4032_{3}$	$0.0310_2$	
-0.7245	$0.5282_{1}$	$-1.3716_2$	$0.1933_9$			Total	15	142.96343		
SG-L/R 10/10, F	PO = 6  vs.  FFT/NF	P = 7								
0.09077	$0.0928_{9}$	$0.9772_{3}$	$0.3462_{6}$	$0.9962_{7}$	0.20248	Model	2	142.4304 <sub>5</sub>	71.2152 <sub>3</sub>	1737.0225 <sub>6</sub>
1.61726	1.4603 <sub>6</sub>	$1.1074_{4}$	0.28817	•	-	Error	13	0.53298	0.041	_
$-0.6160_2$	1.4638 <sub>3</sub>	$-0.4208_{3}$	0.68075			Total	15	142.9634 <sub>3</sub>		
	PO = 6 vs. FFT/NF		-					,		
0.06407	0.064	1.00113	0.3350 <sub>3</sub>	$0.9982_{4}$	$0.1390_{5}$	Model	2	142.71208	71.35604	3690.49976
3.25436	0.57119	5.69753	< 0.0001	-	-	Error	13	0.25136	0.01934	
$-2.2566_{1}$	0.57286	$-3.9391_{9}$	0.0017			Total	15	142.96343	•	
-	= 2 vs. SG-L/R 2/									
$5.3\times10^{-5}$	$9.5 \times 10^{-4}$	0.05605	0.95615	1	$0.0020_{6}$	Model	2	142.9633 <sub>8</sub>	71.48169	$1.7\times10^7$
$0.9706_{9}$	0.00323	300.94135	< 0.0001		3	Error	13	$5.5 \times 10^{-5}$	$4.2 \times 10^{-6}$	
$0.0292_{1}$	0.00327	8.93143	< 0.0001			Total	15	142.96343		
•	= 2 vs. SG-L/R 6/	_								
-0.04681	0.06748	-0.69365	0.50011	$0.9983_2$	$0.1359_{6}$	Model	2	142.72313	71.36156	3860.51452
1.86449	0.35973	5.18298	$1.8 \times 10^{-4}$		0	Error	13	0.2403	0.01848	
-0.84909	0.35834	$-2.3695_3$	0.03397			Total	15	142.9634 <sub>3</sub>		
	PO = 2 vs. SG-L/R	_	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,				-			
0.05555	0.07169	0.77474	0.45235	$0.9978_{1}$	0.15521	Model	2	142.6502 <sub>8</sub>	71.32514	2960.90427
3.64342	1.0880 <sub>6</sub>	3.3485 <sub>5</sub>	0.00524	1	1	Error	13	0.31316	$0.0240_9$	
$-2.6409_8$	1.0889	$-2.4253_8$	0.03059			Total	15	142.9634 <sub>3</sub>		
	PO = 2 vs. SG-L/R									
0.04581	0.05784	0.79213	0.4425	$0.9985_{8}$	0.12488	Model	2	142.76067	71.38034	4576.48592
2.67923	0.40688	6.5845 <sub>8</sub>	< 0.0001			Error	13	0.2027	0.0156	
$-1.6779_5$	0.40784	$-4.1142_5$	0.00122			Total	15	142.9634 <sub>3</sub>	3.0100	
-	= 4 vs. SG-L/R 2/	-	3.0012					1 12.000 13		
$6.7 \times 10^{-4}$	0.00103	0.64834	0.52805	1	$0.0022_{1}$	Model	2	142.96337	71.48169	$1.5\times10^7$
0.9702 <sub>9</sub>	0.00347	279.66333	< 0.0001	•	0.00221	Error	13	$6.4 \times 10^{-5}$	$4.9 \times 10^{-6}$	1.0 / 10
0.02958	0.00352	8.4069 <sub>3</sub>	<0.0001			Total	15	142.9634 <sub>3</sub>	1.5 / 10	
-	= 4 vs. SG-L/R 6/	-	-0.0001			10141	15	1 12,505 13		
$-0.0685_9$	0.06508	-1.05394	0.3111	0.9985	0.12846	Model	2	142.7489	71.37445	4325.01123
2.1101	$0.3750_{6}$	5.62597	<0.0001	0.5505	0.12010	Error	13	0.21454	40.0165	1323.01123
-1.0928	0.37343	$-2.9264_1$	0.01179			Total	15	142.9634 <sub>3</sub>	10.0103	
	0.57543 PO = 4 vs. SG-L/R		0.01179			iotai	1.3	142,30343		
0.0083 <sub>6</sub>	0.0865 <sub>6</sub>	0.0965 <sub>5</sub>	0.92455	0.9972	0.17564	Model	2	142.56245	71.28123	2310.96922
3.6489 <sub>1</sub>	1.5010 <sub>1</sub>	2.43097	0.92435	0.3372	0.17304	Error	13	0.40098	0.03084	2310.30322
3.6489 <sub>1</sub> -2.6436 <sub>9</sub>	-		-			Error Total	15	0.4009 <sub>8</sub> 142.9634 <sub>3</sub>	0.05084	
5	1.5009 <sub>8</sub>	-1.7613	0.1016 <sub>7</sub>			IUIdI	13	142.30343		
	PO = 4 vs. SG-L/R		0.9270	0.9988	0.1140	Model	2	142 7017	71 2059	5407.0922
$-0.0114_7$	0.0549 <sub>6</sub>	$-0.2086_7$	0.83794	0.9988	0.1149 <sub>1</sub>	Model		142.7917 <sub>8</sub>	71.3958 <sub>9</sub>	3407.0922
3.47249	0.47444	7.3192	<0.0001			Error	13	0.1716 <sub>5</sub>	0.0132	
$-2.4723_{7}$	$0.4754_2$	$-5.2003_9$	$1.7 \times 10^{-4}$			Total	15	$142.9634_3$		

ESD: estimated standard deviation; df: degrees of freedom; SS: sum of squares; MS: mean squares.

validated, using one component system. The optimization starts by standard smoothing procedure, including the SG and FFT methods. The polynomial order varied within two-six. The number of points from left and right (L/R) side of the curve are within 2/2-22/22(SG method) and from 2 to 9 for FFT method, respectively. The observed frequencies within the 200-30 cm<sup>-1</sup> region are summarized in Tables 1 and 2, respectively. The results for  $v_i^{(j)}$  and  $Av_i^{(j)}$  are analysed by Student's t-test (Table 3). The obtained p values are within 0.007-0.0001 by Fourier (FFT) smoothing (NP 3 and 5) method. P=0.36 is obtained at FFT and NP=9. The corresponding p values by SG method and polynomial order 2 at L/R within 2/2-18/18 are within 0.052–0.0004, respectively. The calculated pand t-data (Table 3) are compared with tabulated data at 99% confidence level, so as to verify the absence of statistically significant differences. The data clearly show that the application of the individual function to the different complicated spectroscopic patters appear suitable for such spectroscopic analysis. It must be noted that the polynomial order weakly effects to the obtained peak positions and the integral intensities (Fig. 2, Table 3). In contrast the increasing of the number of points L/R leads to the decreasing of the obtained  $A\nu_i^{(j)}$  and  $A\nu_i^{(j,k)}$  values. Moreover are obtained different dependences for the determination of the  $A\nu_i^{(j)}$  and  $\nu_i$  (Table 5, Fig. 5). These results assumes that for here analysed systems, the best correlation between original patterns and smoothed curves are obtained using FFT method with number of points 3 or SG method at polynomial order 2 and L/R 2/2–10/10, respectively. The accuracy, repeatability and precision are also shown in the Table 1.

The frequency assignment (Table 2) is based on the obtained crystallographic data. Typical for all **(1)–(5)** systems is the observed H-bond deformations (Scheme 1) within 180–111 cm<sup>-1</sup> (5.4–3.3 THz). The corresponding skeletal modes are found within 103–60 cm<sup>-1</sup> (3.1–1.8 THz). The torsion mode in of entire side chain about the aromatic system in **(5)** is observed at 55 cm<sup>-1</sup> (1.7 THz), respectively. The first group of peaks are characterized

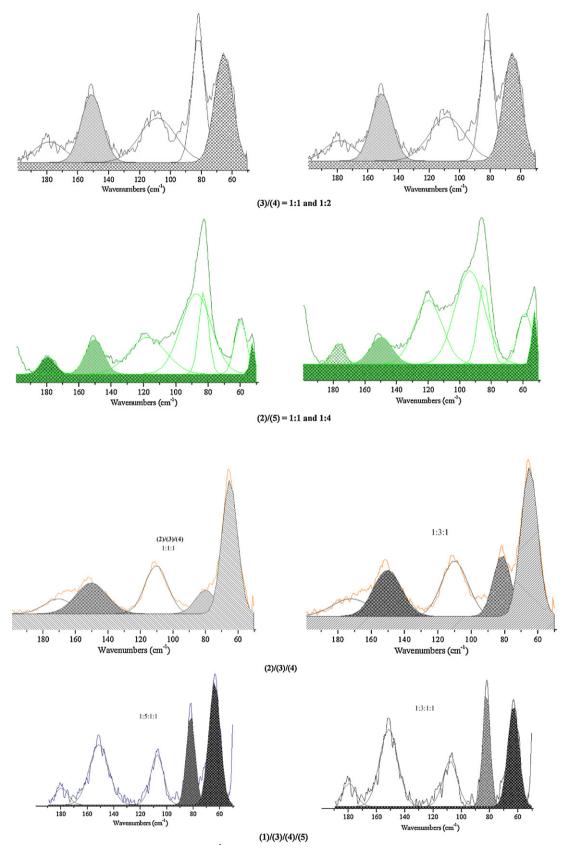
Scheme 1. Dimer and linear hydrogen bond associates of the sulfonamide group and the chain motif formed with anti and syn O acceptor atoms.



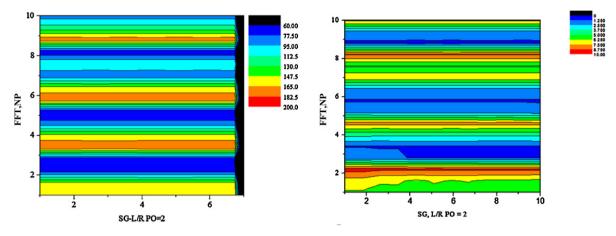
**Fig. 3.** Solid-state Raman spectras of the binary and *n*-component mixtures at different molar ratios.

with a broad character, and relatively low-intensity. In contrast, the corresponding skeletal vibrations are characterized with relatively sharp profile, thus making this group of frequencies as most appropriated for the quantitative determination. On the other side, the observed overlapping effects within the region of 3.1–1.8 THz, difficult the quantitative analysis by the isolated mode, characteristic for each of the studied compounds. For the identification of the solid (including crystalline) materials, the strong individual profile of the spectroscopic patterns within THz-region, allows unambiguously determination of the chemicals, depending of the type of hydrogen bonds, the space system for the crystals, the number of the molecules per unit cell and more. In the case of (5), the complex character of the Raman patters is result of the presence of both types of intermolecular hydrogen bonds, anti and syn O (Scheme 1) [51]. In such cases the individual approach for mathematical interpretation of the observed frequencies appears obligatory strongly depending of the intensity of the excitations, level of overlapping effect, broad profile of the curves and more. Similar to the quantitative analysis within mid-IR region by IRand Raman spectroscopy [23-31], the strong intensive and well defined non-overlapped peaks result to the lower *LODs* values. For the quantitative analysis of **(4)** and **(5)** in the mixtures with **(1)** and **(3)**, the best *LODs* values are obtained, using the strong intensive peaks at  $72 \, \mathrm{cm}^{-1}$  and  $55 \, \mathrm{cm}^{-1}$ , respectively. The  $Av_i^{(j,k)}$  are obtained, using the excitations of the H-bond deformations. Independently of their relatively low intensities, the well defines characterized and low-level of overlapping effect result to the lowest achieved data for *LODs*.

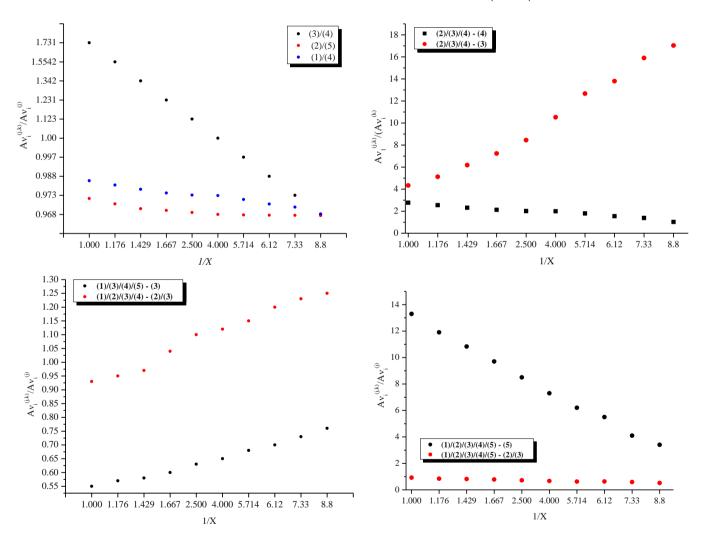
The excitations used for the quantitative determinations of the different mixtures are: (1)/(4):  $v_1 = 60 \pm 0.1 \text{ cm}^{-1}$ ,  $v_2 = 72 \pm 0.1 \text{ cm}^{-1}$  (1); (2)/(5):  $v_1 = 153 \pm 0.2 \text{ cm}^{-1}$ ,  $v_2 = 55 \pm 0.4 \text{ cm}^{-1}$  (5); (3)/(4):  $v_1 = 157 \pm 0.3 \text{ cm}^{-1}$ ,  $v_2 = 72 \pm 0.4 \text{ cm}^{-1}$  (3); (2)/(3)/(4):  $v_1 = 62 \pm 0.3 \text{ cm}^{-1}$ ,  $v_2 = 72 \pm 0.4 \text{ cm}^{-1}$  (3) and  $v_2 = 144 \pm 0.2 \text{ cm}^{-1}$  (4); (1)/(3)/(4)/(5):  $v_1 = 62 \pm 0.3 \text{ cm}^{-1}$ ,  $v_2 = 85 \pm 0.2 \text{ cm}^{-1}$  (3); (1)/(2)/(3)/(4):  $v_1 = 62 \pm 0.3 \text{ cm}^{-1}$ ,  $v_2 = 83 \pm 0.2 \text{ cm}^{-1}$  (2)/(3); (1)/(2)/(3)/(4)/(5):  $v_1 = 62 \pm 0.3 \text{ cm}^{-1}$ ,  $v_2 = 83 \pm 0.2 \text{ cm}^{-1}$  (2)/(3); (1)/(2)/(3)/(4)/(5):  $v_1 = 73 \pm 0.3 \text{ cm}^{-1}$ ,  $v_2 = 55 \pm 0.4 \text{ cm}^{-1}$  (5). The obtained patterns of the individual drugs and the mixtures (Figs. 2 and 4) are procedure by the non-linear curve-fitting method, using the



**Fig. 4.** Curve-fitted solid-state Raman spectra within the  $200-30\,\mathrm{cm}^{-1}$  of the solid mixtures of compounds studied at different molar ratios; curve-fitted spectroscopic patterns after the baseline correction method, by non-linear multipeak Lorenzian–Gaussian function at ratio 1:1; *A* is the total area under the curve from the baseline centre of the peak;  $w^2$  "sigma", approximately 0.441 the FWHM; w/2 is the standard deviation, respectively.



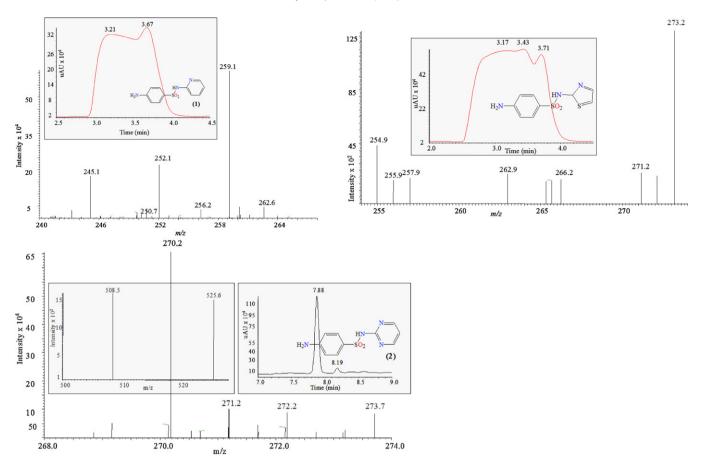
**Fig. 5.** 2D image plot of the statistical correlations between the methods towards the  $v_i^{(j)}$  and  $Av_i^{(j)}$  values.



**Fig. 6.** The straight-line plot from the regression analysis of the *n*-component mixtures.

Lorenzian-Gaussian mixed [23–32] functions at ratio 1:1 at 2000–4000 iterations. The obtained p values around 0.0042 indicate difference between means at 99% and below the critical value of 0.05. Regression analysis (Fig. 7) of the data gave a straight-line calibration plots (Table 4). The obtained LODs for (2)/(3) are 0.010 mole fraction. This result indicates, unambiguously the capability and perspectives in front the quantitative analysis within THzregion. The relatively high LODs value for 0.072 for the analysis

of (1) in system (1)/(4) is explain with the complicated individual spectroscopic patterns of the compounds, characterizing with the broad and relatively overlapped frequencies (Fig. 3). For the n-component mixtures with n=3–5, the obtained data depends strongly of the chosen mode. As can be seen (Table 4, Figs. 3 and 4) the dependence of  $Av_i^{(j...n)}/Av_i^{(j)}$  vs. the mole fraction of the determining substances, result to  $r^2$  values within 0.99844–0.98843, respectively. Comparing the highest obtained value for the n=5



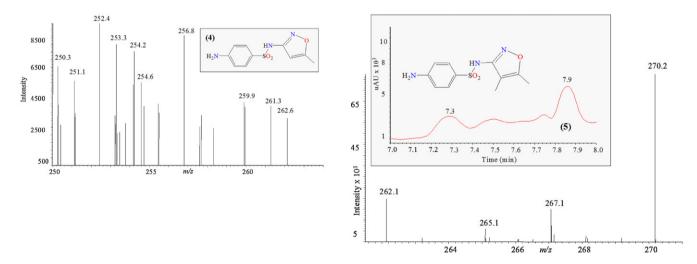


Fig. 7. HR HPLC ESI-MS/MS data of (1)–(5), respectively.

(i.e. system (1)/(2)/(3)/(4)/(5), towards the determination of (5)) and this for n=2 ((3)/(4), analysing the (3)), only a decreasing of the  $0.1_5\%$  is obtained. This result in addition illustrates the great capability of the method for detection of multicomponent mixtures. It should however taking into account that the spectroscopic patterns of the mixtures for the system n=5 ((1)/(2)/(3)/(4)/(5)) are characterized with the strong intensive frequencies and low degree of overlapping effect. It is interesting to note as well that

the analysis of the systems n=4 ((1)/(2)/(3)/(4)–(3)/(2)) and n=5 ((1)/(2)/(3)/(4)/(5)–(3)/(2)) results to the reliable data for  $r^2$  of 0.9917<sub>5</sub> of 0.9884<sub>3</sub>, respectively. The observed overlapping effect of corresponding excitations of the skeletal modes and the torsion of entire side chain about the aromatic system result to the determination of the compounds (2)/(3) as sum. In this case, the obtained relatively lower value of  $r^2$ , is explain additionally with the shifting effect of the used for the quantitative analysis excitations at

about  $\pm 3$  cm<sup>-1</sup>. Such effect result to the increasing of the error of the used mathematical methods for determination of the  $v_i$ , respectively. The demonstrate, sensitivity of the obtained quantities using the vibrations within THz-region must be done carefully taking into account as well the factor, signal to noise (S/N). Such for example, systems (1)/(4) (Fig. 1) and (1)/(2)/(3)/(4)/(5) (Fig. 4) are characterized with low S/N ratio, thus resulting to application of the FFT and SG methods ate relatively high polynomial order and NP. As can be seen from the obtained  $r^2$  values the error effect significantly influenced the  $Av_i$  values at about 0.14%, both applying the non-linear and MLR methods (below). The obtained parallel data from the multiple linear regression and ANOVA test for MLR are summarized in Table 5 and visualized in Fig. 5, respectively. The obtained  $r^2$  values within the  $0.9999_8$ – $0.9988_6$ , especially determining the  $A\nu_i$  values, prove additionally that there is no one perfect one mathematical method to fit the experimental data-set. As obtained for example to the obtained  $r^2$  value by the non-linear peak fitting methods of  $0.9998_9$  for determining the  $Av_I$ , corresponds a  $0.9968_6$  by the MLR method. The obtained difference of the 0.3%, indicate dominantly the application of individual functional simulations.

### 3.2. HPLC tandem ESI-MS/MS mass spectrometry

The correlations between the results in samples with different amounts of (1)-(5) for all of studied systems, obtained by spectroscopic Raman and HPLC ESI MS/MS technique demonstrate good agreement with correlation coefficients > 0.9998. HPLC ESI MS/MS analyses of the isolated compounds were performed using the procedures described [31] for quantitative determination. The corresponding m/z values of each of the samples in the isolated components as well as at the binary mixtures are shown in the same figure as well as the relatively abundance times in corresponding chromatograms. The observed peaks m/z at 259.1, 263.8, 264.2, 262.6, 270.2 correspond to the cations of the (1)-(5), i.e.  $[C_{11}H_{12}N_3SO_2]^+, [C_{10}H_{11}N_4SO_2]^+, [C_9H_9N_3S_2O_2]^+, [C_{10}H_{11}N_3SO_3]^+$ and  $[C_{11}H_{14}N_3SO_3]^+$  with the molecular weights of 259.1, 262.8, 264.3, 262.8, and 270.9 respectively. The corresponding values in the binary mixtures are weak effects. Only in the systems (1) and (2), the observed peaks at higher values of m/z 518.4 and 525.6 which could assigned to the stable associates in gas phase [57,58], most probably related to the typical for pyridinium systems  $N_{(Pv)} \cdots H \cdots N$ -dimers (Figs. 6 and 7).

# 4. Conclusions and outlook

In this paper, we have outlined the possibilities of the vibrational analysis within the THz-region towards the quantitative elucidation, determination and identification of the individual drugs and solid n-component mixtures. The solid-state Raman spectroscopy and the non-linear mathematical methods for interpretation of the spectroscopic patterns result to low LODs. Perhaps most importantly, it is essential to nightlight the new perspectives in front IR-, Raman and THz-spectroscopy within THz-region for complete assignment of the optical phenomena, unambiguous materials identification in solid-state [1-21]. The advantages for non-destructive materials identification and application in the interdisciplinary technological fields such as development of methods for security, environmental inspection, detection and protection are towards both qualitative and quantitative analysis. The results, demonstrated as well, the advantages of the solid-state Raman spectroscopy, using the excitations of H-bond deformations, skeletal modes, and/or lattice vibrations within THz-region, and the application of the additional mathematical methods for spectroscopic curve procedure, resulting to low LODs. Especially for the analysis of the complex patterns of *n*-component solid mixtures is shown remarkable for the vibrational spectroscopy LODs of the Raman spectroscopy 1.34%. The analysis of the five model systems of the sulfonamide drugs as isolated chemicals and in the *n*-component mixtures, show *LODs* within 0.010–0.012 mole. The dependences of integral area under the curves  $AP^{(j \cdots n)}/AP^{(j)}$  vs. the mole fraction of the determining substances result to regression factor  $r^2$  0.9984<sub>4</sub>-0.9884<sub>3</sub> for n=5 and 0.9998<sub>9</sub> for n=2, respectively. It should taking into account that the application of the THz-spectroscopic range, for analysis requires an individual functional approach for elucidation and characterization. Thus, the performed parallel to the non-linear approach, the multiple linear regression analysis show  $r^2$  values  $0.9999_8-0.9988_6$ , respectively. The highest one is obtained determining the  $v_i$  of binary mixture, respectively. The analysis of the AP, however using the non-linear methods results to better factor (0.9998<sub>9</sub>) about 0.14% for tricomponent solid mixture. These results, illustrate the large potential for further investigations of the solid-mixtures towards validation and defining of the advantages and limitations of the analysis within THz-region for identification and especially for quantitative determination.

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